The spread of behaviour from widespread continuum damage failure to highly localised creep crack growth, triggered by variation of material ductility in superalloys, can be predicted by the same technique.

The same method has been used to predict the results of creep crack growth behaviour in a welded pressurised pipework branch connection; and, the CDM predictions have been shown to agree with the results of well-established C^* prediction methods based on non-linear fracture mechanics.

A simple CDM method of analysis has been used in all cases. The only difference being the material, applied stress levels and stress states, and consequently the physically based constitutive equations selected.

It is advocated that with the increasing speed, and data storage capacity of computer workstations such calculations will soon be trivial provided: (a) Accurate materials test data is available. (b) Techniques are available to select the relevant physical models for creep deformation and damage, and to fit the models to the data.

When such facilities are available, design by analysis will have much appeal over design by code. In this way, many aspects of the three barriers to progress, given in the introduction, will be removed; hence much of the present conservatisms may be confidently removed.

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9. NOMENCLATOR

- A Material constant (1/h)
- B Material constant (1/MPa)
- C Material constant, dimensionless
- C* Steady state creep characterising parameter (MPa m/h)
- Ductility factor (=1/3 ε_f), dimensionless
- G Material constant (mm/h)
- H Primary creep state variable, dimensionless
- H* Material constant, dimensionless
- h Material constant (MPa)
- K Material constant (1/MPa h^{m+1})
- k_c Material constant (1/h)
- Material constant, $(1/MPa^{x}h^{m+1})$
- m Material constant, dimension less
- n Stress exponent in creep law, dimensionless
- p Internal pressure (MPa)
- q Material constant, dimensionless
- s_{ij} Deviatoric stress, $s_{ij}=\sigma_{ij}-\delta_{ij} s_{kk}/3$ (MPa)
- t Time (h)